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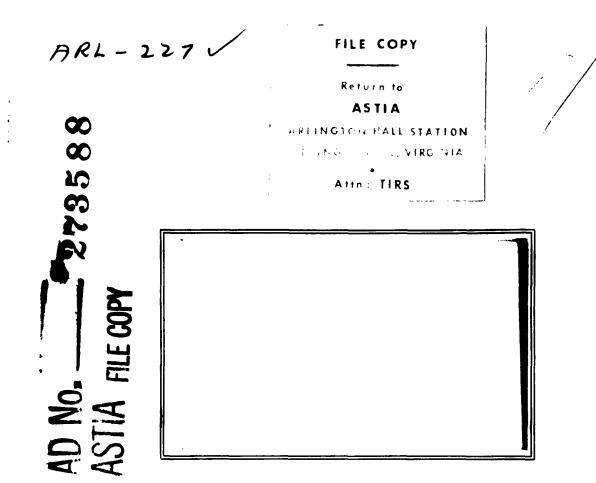
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MONITORING	AGENCY DOCUMENT	No	
ASTIA DOCUM	MENT No. AD		
CONTRACT A	AF 61(052)-170	TN 5.	

TECHNICAL NOTE #5

Computation of the Emissivity
of a Cylindrically Symmetric Light Source
from Measurements of the Projected
Intensity Profile

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July 31, 1961

The research reported in this document has been supported in part by the

AERONAUTICAL RESEARCH LABORATORY

of the OFFICE OF AEROSPACE RESEARCH, UNITED STATES AIR FORCE

through its European Office

COMPUTATION OF THE EMISSIVITY OF A CYLINDRICALLY SYMMETRIC LIGHT SOURCE FROM MEASUREMENTS OF THE PROJECTED INTENSITY PROFILE

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A method is described for computing the emissivity  $\frac{f(r)}{f(r)}$  (red.) of a cylindrically symmetric, optically thin light source, when the projected intensity profile  $\frac{f(r)}{f(r)}$  dy is known from experiment. The unknown function  $\frac{f(r)}{f(r)}$  is taken as a series expansion in terms of orthogonal polynomials, and it is shown how the expansion coefficients can be determined from  $\frac{f(r)}{f(r)}$ . This procedure yields a least-squares smoothed approximation for  $\frac{f(r)}{f(r)}$ .

Let f(r) be the emission coefficient (emission per unit area) of a cylindrically symmetric, optically thin light source of unit radius. Side-on measurements of the emission give the projected intensity profile I(x), which is related to f(r) by

$$I(\mathbf{x}) = \int_{-\sqrt{1-\mathbf{x}^2}}^{\sqrt{1-\mathbf{x}^2}} \mathbf{f}(\mathbf{r}) d\mathbf{y} = 2 \int_{\mathbf{x}}^{1} \frac{\mathbf{f}(\mathbf{r}) \cdot \mathbf{r} d\mathbf{r}}{(\mathbf{r}^2 - \mathbf{x}^2)^{\frac{1}{2}}}$$
(1)

The inversion of eq. (1), giving f(r) in terms of T(x), is

$$f(\mathbf{r}) = -\frac{1}{2\pi} \int_{\mathbf{r}} \frac{I(\mathbf{x}) c^{2}}{(\mathbf{x}^{2} - \mathbf{r}^{2})^{2}} = -\frac{2}{2\pi} \int_{\mathbf{r}^{2}} \frac{I(\mathbf{x}) \mathbf{x} d\mathbf{x}}{(\mathbf{x}^{2} - \mathbf{r}^{2})^{2}}.$$
 (2)

The problem of detarmining  $f(\mathbf{r})$  when  $f(\mathbf{x})$  is known from expriment. has been treated by several authors,  $f(\mathbf{r})$  mostly by some method of strip integration. An accurate numerical method has been given by Bockaston.

The x-axis is divided in a number of equal intervals, and a third-degree polynomial is fitted to the I(x) curve within each interval. Eq. (2) is used, and a matrix  $A_{ik}$  is obtained that transforms a set of values of I to values of f,

$$f(r_i) = \sum_{k} A_{ik} I(x_k).$$
 (3)

Bookasten also discusses the influence of random errors in the values of I(x).

The method described in this note should be advantageous whenever the I(x) curve has a more or less irregular shape, and a properly smoothed approximation to f(r) is desired. The unknown function f(r) is expanded in a series of orthogonal polynomials. The expansion coefficients can be determined from I(x), and in this way a least-squares smoothed approximation to f(r) can be found directly.

A few general consequences of eqs. (1) and (2) are of interest. Obviously I(x) is an even function, and we consider the interval  $0 \le 1 \le 1$  only. The behavior of f(r) near r=1 is very sensitive to the behavior of I(x) near x=1. If I(x) is projectional to  $(1-x)^b$  near x=1, then f(r) will be proportional to  $(1-r)^{b-\frac{1}{2}}$  near r=1. For instance, b=0.49, b=0.5, and b=0.51 correspond to infinite. Finite and zero values of f(1), respectively. Further, it is seen from eq. (2) that a discontinuity in I'(x) at x=0 implies an infinite value of I'(0). We will assume that the functions I'(x) and I'(r) are finite, to that I''(0) = 0, and I'(1) = 0 (with  $b \ge \frac{1}{2}$ ).

We now choose to fit in even polynomial  $f_{ij}(\mathbf{r})$ , of legree  $G_i$ , to  $f_{ij}(\mathbf{r})$ , in such a way that the error squared, integrated over the cross-section  $\mathbf{r} \leq 1$ , is within a thus,

$$\int_{0}^{1} (\mathbf{f} - \mathbf{f}_{\mathbf{M}})^{2} \mathbf{r} d\mathbf{r} = \min., M \text{ fixed.}$$
 (4)

The orthogonal polynomials suitable for this purpose are the Legendro polynomials  ${}^4$   $P_m(t)$ , with  $t=2r^2-1$ . The first few of these are  $P_0=1$ ,  $P_1=2r^2-1$ ,  $P_2=6r^4-6r^2+1$ ,  $P_3=20r^6-30r^4+12r^2-1$ .

They satisfy the orthogonality relation

so that the series expansion of f(r) is

$$f(r) = \sum_{m=0}^{\infty} a_m P_m (2r^2 - 1)$$
 (6)

with

$$a_m = 2(2m+1) \int_0^1 f(r) P_m(2r^2-1) r dr.$$
 (7)

If the series (6) is terminated at m = M, the result is a 2M-degree polynomial  $f_M$ , which satisfies the condition (4).

We substitute the series (6) in eq. (1), integrate term by term, and obtain x)

$$I(x) = \sum_{m=0}^{\infty} 2(2m+1)^{-1} a_m \sin \left[ (2m+1)\cos^{-1} x \right], \tag{8}$$

or, putting  $x = \cos \theta$ ,

$$I(\cos\theta) = \sum_{m=0}^{\infty} 2(2m+1)^{-1} a_m \sin(2m+1)\theta.$$
 (9)

The functions  $U_n(x) = \sin(n \cos^{-1}x)$  are related to the Chebyshov polynomials  $T_n(x) = \cos(n \cos^{-1}x)$ . They satisfy the orthogonality r = 100 tion  $\int_{-1}^{1} U_k U_n (1-x^2)^{-\frac{1}{2}} dx = 0$ , k/n, and vanish at the points  $x = \pm 1$ .  $U_n(x)$  is an even function if n is odd.

It can be shown from eqs. (1) and (7) that

$$2(2m+1)^{-1} a_m = (4/\overline{\nu}) \int_0^{\overline{\nu}/2} I(\cos\theta) \sin(2m+1)\theta d\theta,$$
 (10)

so that eq. (1) (with  $x = \cos\theta$ ) transforms the Legendre series of f(x) into the Fourier series of  $I(\cos\theta)$  (odd sine terms only). It may be noted that the total emission from the light source is

$$2\pi \int_{0}^{1} f(r) r dr = 2 \int_{0}^{1} I(x) dx = \pi a_{0}.$$
 (11)

It is also seen that, if  $f_M(r)$  satisfies the condition (4), then the corresponding function  $I_M(x)$  (the sories (8) terminated at m=M) will be the "best" approximation for I(x), in the sense that the integral

$$\int_{0}^{1} (I - I_{N})^{2} (1 - x^{2})^{-\frac{1}{2}} dx$$

is minimized.

The standard methods of Fourier analysis  $^{5}$  can now be used for determining the coefficients  $a_{n}$ . One possible procedure is as follows: The series (9) is terminated at some m = N:

$$I_{N}(\cos\theta) = \sum_{m=0}^{N} 2(2m+1)^{-1} a_{m} \sin(2m+1)\theta,$$
 (12)

and I, is required to coincide with I in those points in the interval 0.494.8/2 where the first neglected term ( $\sin(2N+3)9$ ) vanishes. These points are

and the soluti is

$$a_m = 2 \frac{2m+1}{2N+3} \sum_{k=1}^{N+1} I(\cos \frac{k\pi}{2N+3}) \sin \frac{(2m+1)k\pi}{2N+3}, m=0, 1...N.$$
 (13)

This result can also be obtained by evaluating the integral (10) by the trapezoidal rule. Eq. (13) is exact if f(r) is an even polynomial of degree 2(N+1) or less, so that the series (6), (8), and (9) contain no terms beyond m = N+1.

With the  $a_m$  given by eq. (13), the 2M-degree polynomial approximation for f(r) becomes

$$f_{M}(\mathbf{r}) = \sum_{m=0}^{M} a_{m} P_{m}(2r^{2}-1) = \sum_{k=1}^{N+1} A_{k}(\mathbf{r}) I(\cos \frac{kT}{2N+3})$$
 (14)

where

$$A_{k}(\mathbf{r}) = \frac{2}{2N+3} \sum_{m=0}^{M} (2m+1) \sin \frac{(2m+1) k\pi}{2N+3} P_{m}(2\mathbf{r}^{2}-1). \quad (M \le N) \quad (15)$$

As an example we consider the function

$$I = (1 - x^2)^2 = \sin^4 \theta, \tag{16}$$

corresponding to

$$f(r) = (8/3\pi)(1-r^2)^{3/2}.$$
 (17)

The coefficients  $a_m$ , computed from eq. (13), are listed in Table 1. The exact  $a_m$ , given by eq. (7) or (10) are entered in the last line. They are

$$a_m = \frac{48}{1} \frac{1}{(2m-3)(2m-1)(2m+3)(2m+5)},$$
 (18)

showing fairly rapid convergence. The convergence is slowest near the points r=0 and r=1, where  $|P_m|=1$ . A seven-point analysis (N=6) is sufficient to reduce the error in f(r) to about 0.0006 for r=0 and 0.001 for r=1.

Table 2 shows the same for

$$I = 1 - x^2 = \sin^2 \theta, (19)$$

corresponding to

$$f(\mathbf{r}) = (2/\pi) (1-\mathbf{r}^2)^{\frac{1}{2}}.$$
 (20)

The exact coefficients a are

$$a_{m} = -\frac{4}{\pi} \frac{1}{(2m-1)(2m+3)},$$
 (21)

so that the convergence is fairly slow. Clearly, the behavior of the function (20) near r=1 cannot be represented accurately by a low-dogree polynomial. However, a seven-point analysis (N=6) suffices to give an error less than about 0.002 for r £0.98.

Experimental measurements will commonly yield I(x) curves with irregular fluctuations, rather than smooth functions of the type (16) or (19). In such cases it should be an advantage of this method that, with a suitable choice of N and M, a properly smoothed f(r) is obtained directly.

The influence of random errors in the values of I(x) can be found as follows. If the error (standard deviation) of I at each point is  $\Delta I$ , eq. (13) gives for the error  $\Delta a_m$  of  $a_m$ ,

$$(\Delta a_m)^2 = 4(\frac{2m+1}{2N+3})^2 (\Delta I)^2 \sum_{k=1}^{N+1} \sin^2 \frac{(2m+1)^2 k k^2}{2N+3} = \frac{(2m+1)^2}{2N+3} (\Delta I)^2,$$

or

$$\Delta a_{m} = \frac{2m+1}{(2N+3)^{2}} \Delta I.$$
 (22)

For the function (19), assuming  $\Delta I = 0.002$  and N = 6, we see from eq. (22) and Table 2 that the error in  $a_5$  is comparable to  $a_5$  itself, so that this source of error is more important than the fairly slow convergence of the Legendre series.

From eq. (14), the error in  $f_1$  is given by

$$(\Delta t_{\rm M})^2 = (\Delta I)^2 \sum_{k=1}^{N+1} [A_k(r)]^2,$$
 (23)

which cannot be expressed in a simple form. We can obtain an estimate for Af, from the expression

$$(\Delta t_{\rm M})^2 = \sum_{\rm m=0}^{\rm M} (\Delta a_{\rm m})^2 P_{\rm m}^2, \tag{24}$$

which would be correct if the  $\triangle a_m$  were uncorrelated.  $\triangle f_M$  will be largest at the points r=0 and r=1, where  $|P_m| = 1$ . We find from eqs. (22) and (24),

$$\Delta r_{M} = \Delta I \sqrt{\frac{(M+1)(2M+1)(2M+3)}{3(2N+3)}}, r=0, 1.$$
 (25)

For intermediate values of r, the error will be smaller, although no simple formula can be given. For instance, for  $r^2 = 0.5$  and N = 6, eqs. (22) and (24) yield  $\Delta f_6 = 5.9 \times (2N+3)^{-\frac{1}{2}}$ I, while the end-point value given by eq. (25) is 21 x (2N+3) I. For N = 10 the factor is 9.0 and 42, respectively.

#### Acknowledgeont

The author is indebted to Dr. K. Bockasten for valuable discussions and comments.

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Table 1

Expansion coefficients  $a_m$  of the function  $(8/3f)(1-r^2)^{3/2}$ , approximate values from eq. (13) with N=0, 1, 3, 6, and (last line) correct values from eq. (18).

n	<sup>a</sup> 0	<sup>a</sup> 1	<sup>a</sup> 2	<sup>a</sup> 3	<sup>a</sup> 4	<b>a</b> 5	<sup>a</sup> 6
0	0.32476						
1	0.33931	-0.44089					
3	0.33957	-0.43660	0.08062	0.00951			
6	0.33953	-0.43657	0.08083	0.01027	0.00306	0.00117	0.00046
(00)	0.33953	-0.43654	0.08084	0.01029	0.00305	0.00124	0.00061

### Table 2

Expansion coefficients  $a_m$  of the function  $(2/\pi)(1-r^2)^{\frac{1}{2}}$ ; approximate values from eq. (13) with N = 0, 1, 3, 6, and (last line) correct values from eq. (21).

<u>r</u>	<b>a</b> 0	<sup>a</sup> .1	a <sub>2</sub>	<sup>a</sup> 3	a. 4	<sup>a</sup> 5	<sup>a</sup> 6	
0	0.4330		·· · · · · · · · · · · · · · · · · · ·					
1	0.4253	-0.2437						
3	0.4245	-0.2538	-0.0580	-0.0216				
6	0.4244	-0.2546	<b>-</b> 0.0603	-0.0277	-0.0154	-0.0089	-0.0044	
(24)	0.4244	-0.2546	-0.0606	<b>-</b> 0.0283	-0.0165	-0.0109	-0.0077	

Rep. No. AD TN 5 TN 5	Field: Physics Monitoring Agency:	COMPUTATION OF THE EMISSIVITY OF A CYLINDRICALLY SYMMETRIC LIGHT SOURCE FROM MEASUREMENTS OF THE PROJECTED INTENSITY PROFILE SOURCE FROM MEASUREMENTS OF THE PROJECTED INTENSITY PROFILE	Date: July 31, 1960 S. I. Herlitz Date: July 31, 1960	ABSTRACT: A method is described for computing the emissivity $f(r)$ ( $r \le 1$ ) of a cylindrically symmetric, optically thin light source, when the projected intensity profile $f(x) = f(r)$ dy is symmetric optically thin light source, when the projected intensity profile $f(x) = f(r)$ dy is symmetric optically thin light source, when the projected intensity profile $f(x) = f(r)$ dy is symmetric optically thin light source, when the projected intensity profile $f(x) = f(r)$ dy is symmetric. Optically thin light source, when the projected intensity profile $f(x) = f(r)$ dy is symmetric. Optically thin light source, when the projected intensity profile $f(x) = f(r)$ dy is symmetric. Optically thin light source, when the projected intensity profile $f(x) = f(r)$ of a cylindrically is symmetric. Optically thin light source, when the projected intensity profile $f(x) = f(r)$ of a cylindrically thin light source, when the projected intensity profile $f(x) = f(r)$ of a cylindrically thin light source, when the projected intensity profile $f(x) = f(r)$ of a cylindrically symmetric. Optically thin light source, when the projected intensity profile $f(x) = f(r)$ of a cylindrically symmetric. Optically thin light source, when the projected intensity profile $f(x) = f(r)$ of a cylindrically symmetric. Optically the cylindrical symmetry $f(x)$ is taken as a series expansion in terms of cylindrical symmetric $f(x) = f(x)$ of a cylindrical $f(x) = f(x$	(DC., Brussels, Relgium	Rep. No. AD TN 5 TN 5	Field: Physics Monitoring Agency: Field: Physics	COMPUTATION OF THE EMISSIVITY OF A CYLINDRICALLY SYMMETRIC LIGHT SOURCE FROM MEASUREMENTS OF THE PROJECTED INTENSITY PROFILE SOURCE FROM MEASUREMENTS OF THE PROJECTED INTENSITY PROFILE	Date: July 31, 1960 S. I. Herlitz Date: July 31, 1960	ABSTRACT: A method is described for computing the emissivity $Rr$ ) ( $r \le 1$ ) of a cylindrically symmetric, optically thin light source, when the projected intensity profile $(x) = f(r) dy$ is shown from experiment. The unknown function $Rr$ is taken as a series expansion in terms of corhogonal polynomials, and it is shown how the expansion coefficients can be determined from $R(x)$ . This procedure yields a least-squares smoothed approximation to $R(r)$ .	IDC, Brussels, Belgium USAF, European Office, ARDC, Brussels, Belgium
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